

# **STATUS of BBC DESIGN and ENGINEERING : PRELIMINARY RESULTS**

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# Outline

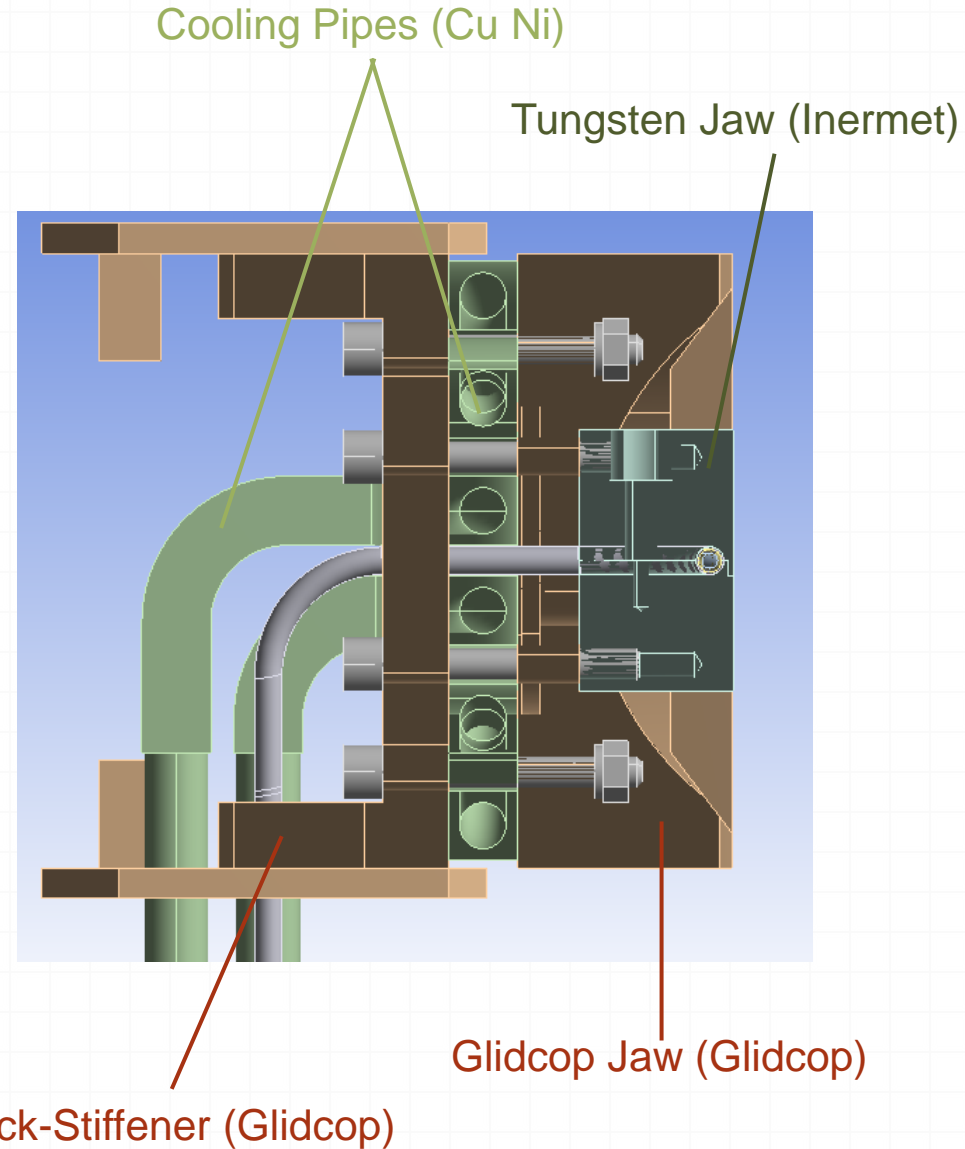
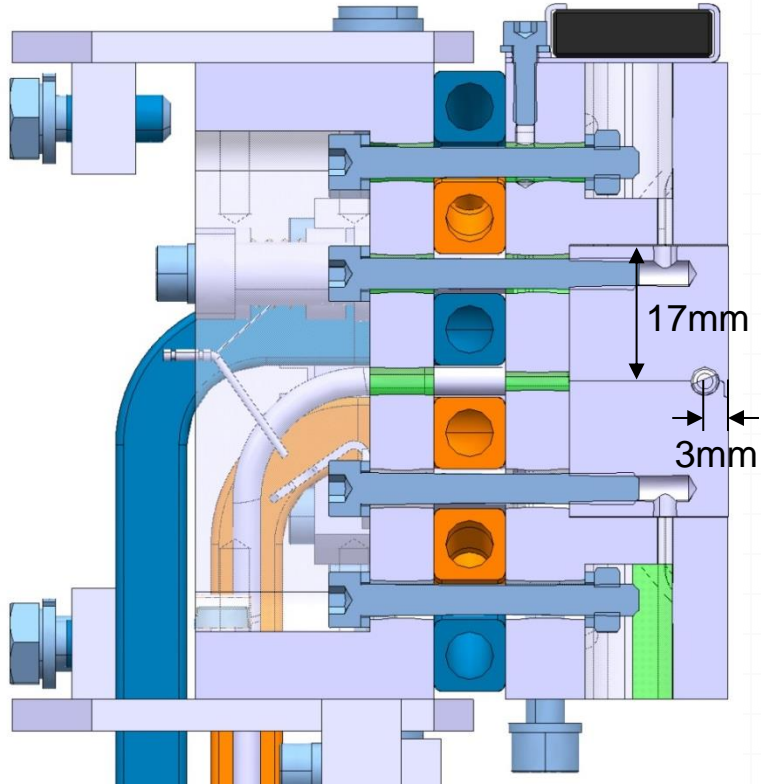
## Beam-Beam compensator:

Decreasing the influence of a beam on the other using electrified wire in some TCTP collimators

### Specifications:

- Re-use **nearly 100%** of existing TCTP design
- Electrified wire as close as possible to the beam axis:  
distance the center of the wire - the surface of the jaw **<3mm**
- Maximum diameter of the copper **2mm**
- Maximum input current: **350A DC**
- If possible, **2 wires** (1 working – 1 spare)

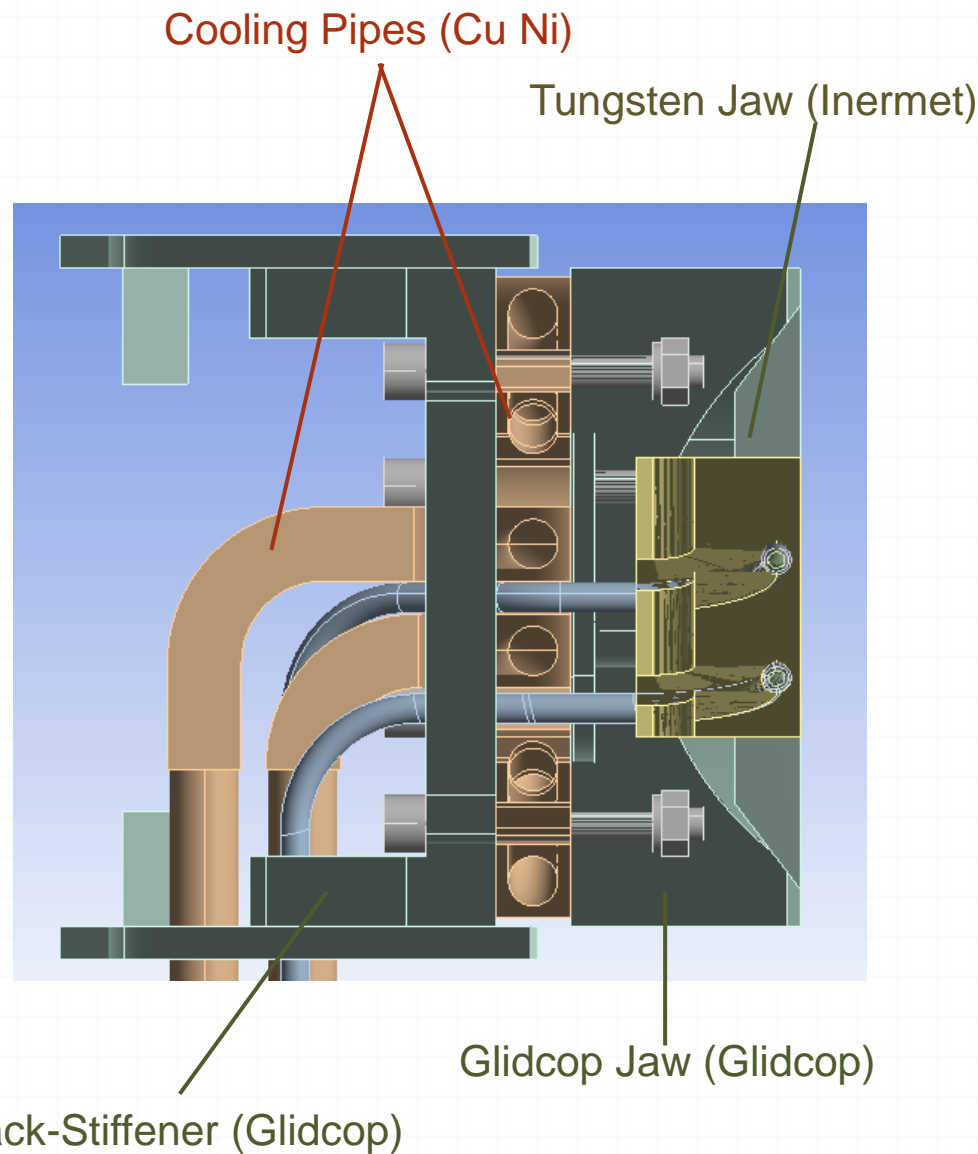
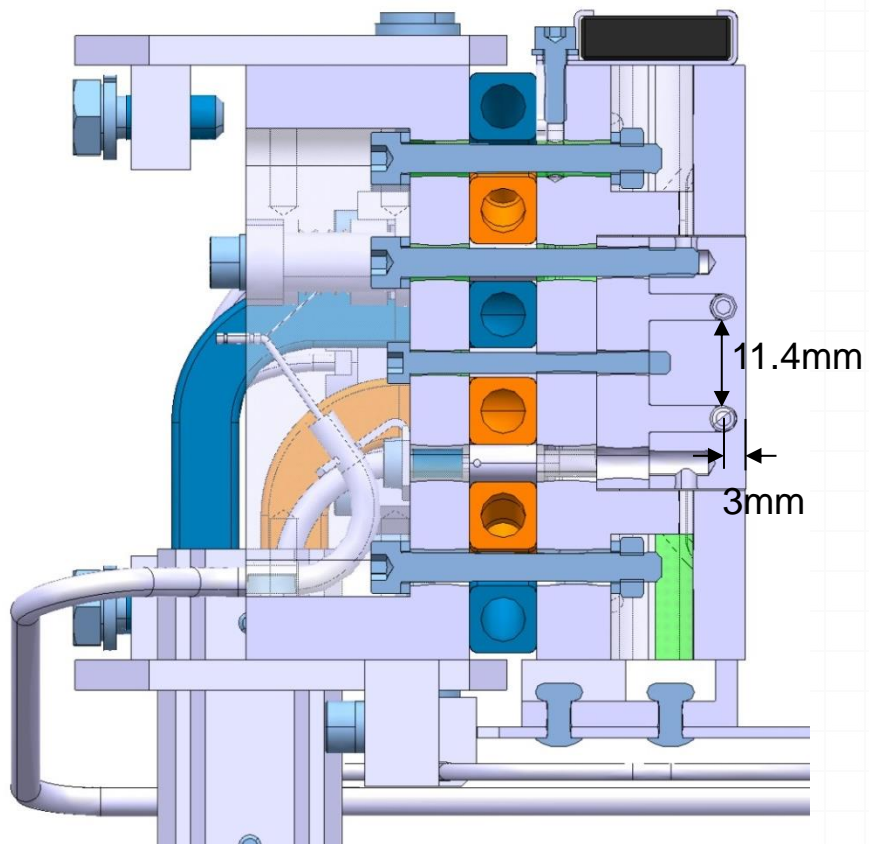
# 1 Wire Design



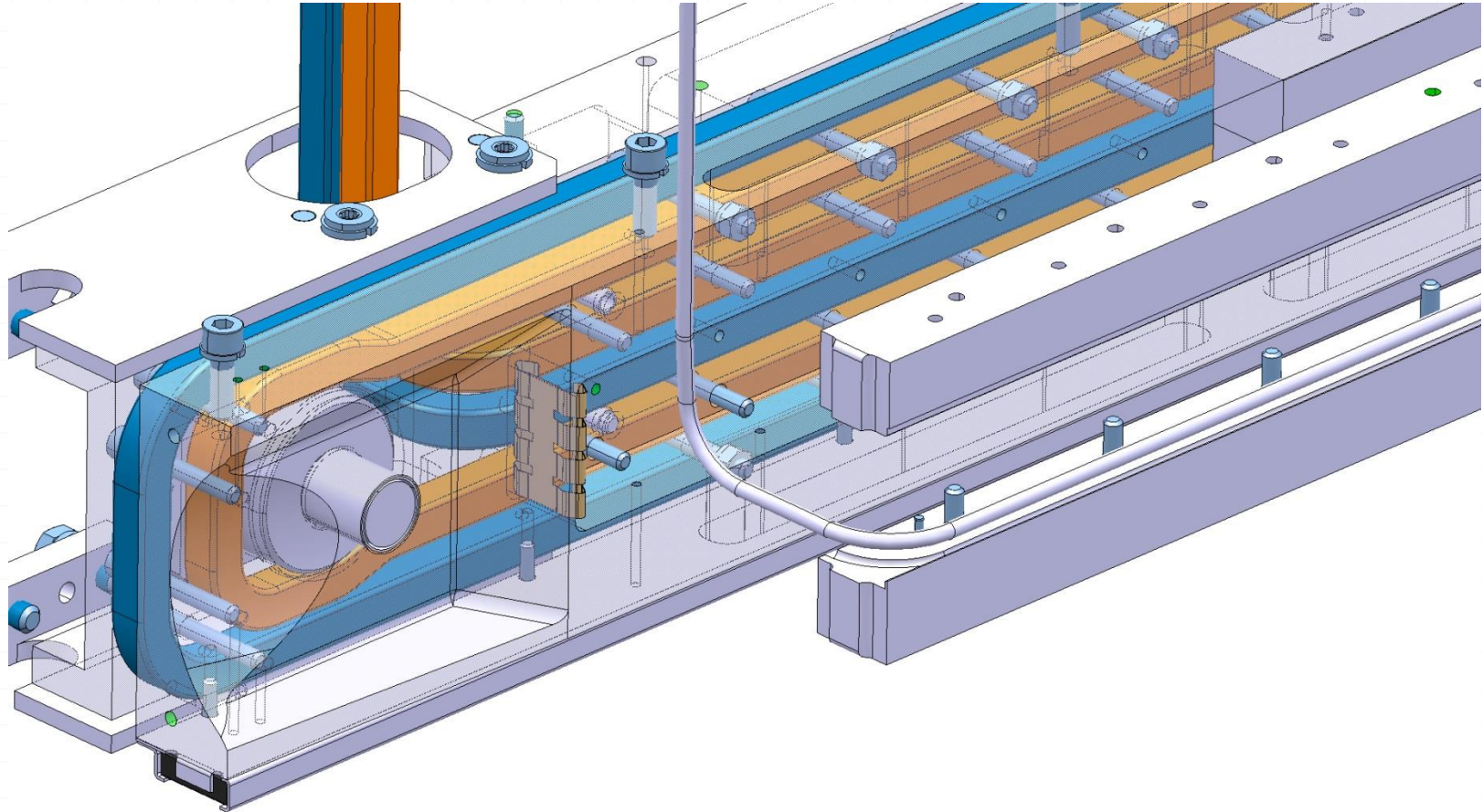
# 2 Wires Design

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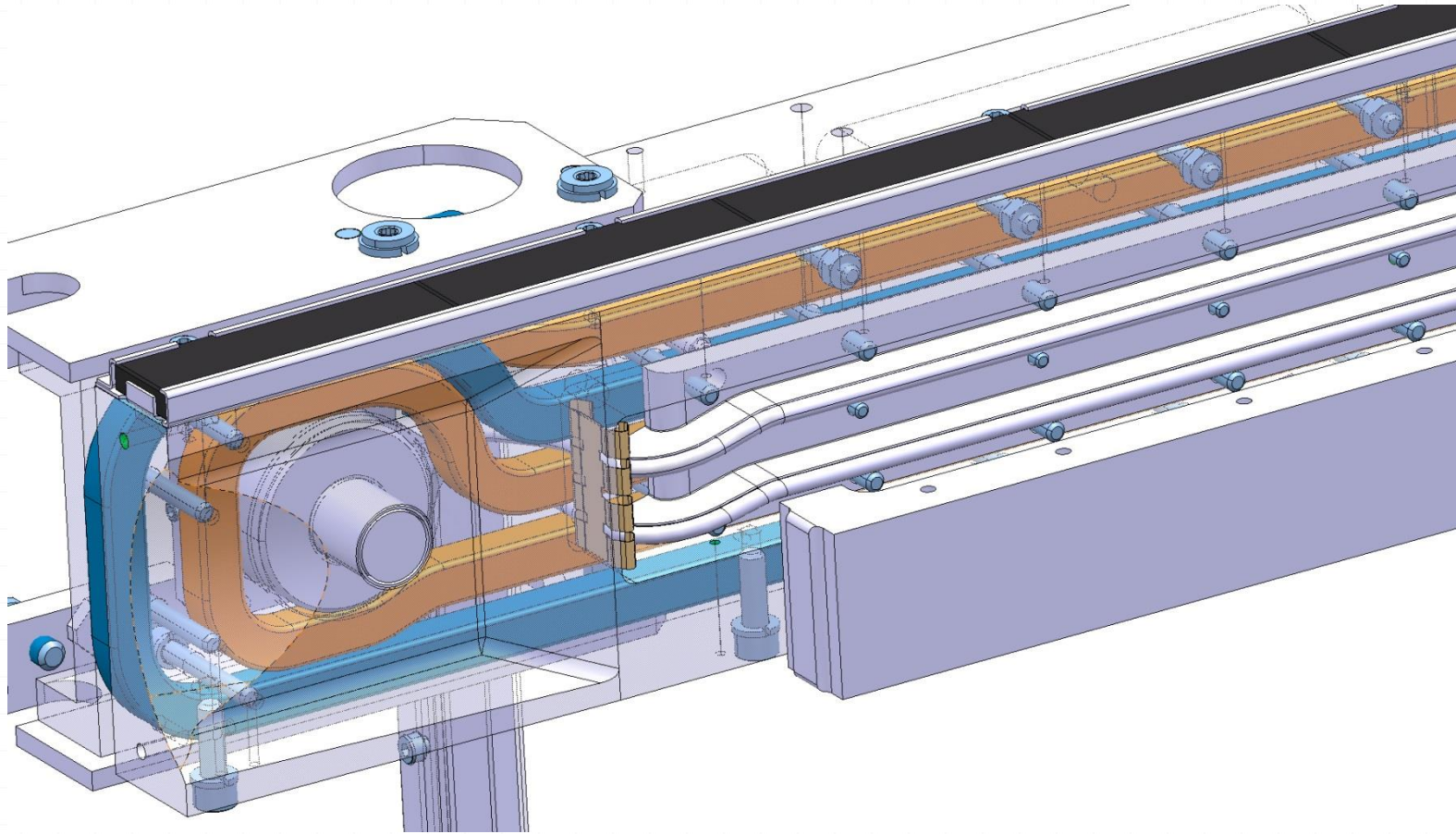


# 1 Wire Design





# 2 Wires Design



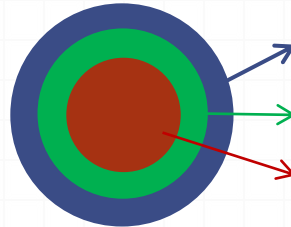
# Wire

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## Thermocoax wire

3 Layers  
Total diameter : 3.6mm



Stainless Steel – Thickness 0.3mm

Magnesium oxide – Thickness 0.5mm

Copper – Diameter 2mm

## Electrical properties :

Magnesium Oxide layer → perfect electrical insulator

Copper → very good electrical conductor

**Maximum admissible temperature (estimated by Thermocoax, not tested):  $\approx 400^{\circ}\text{C}$**   
(under testing by A. Ravni)



# TCTP Thermal Load

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## TCTP without BBC

1h Beam Life Time ( $8.6e8$  p/s) on each Jaw : 418.4W

## TCTP with BBC

Heat generation due to Joule effect in the wire with 350 A :

$2.11e8$  W/m<sup>3</sup> (at 300°K)

## Total thermal power dissipation:

1 Wire design at 300°K :  $940$  W +  $418$ W from beam

2 Wires design at 300°K :  $986$  W +  $418$ W from beam

**BBC : adds more than twice the 1h BLT thermal load  
optimistically assuming RT Cu electric resistivity**



# Thermal simulation : wire cooled only in Jaw

Calculation for both designs: 1 and 2 wires

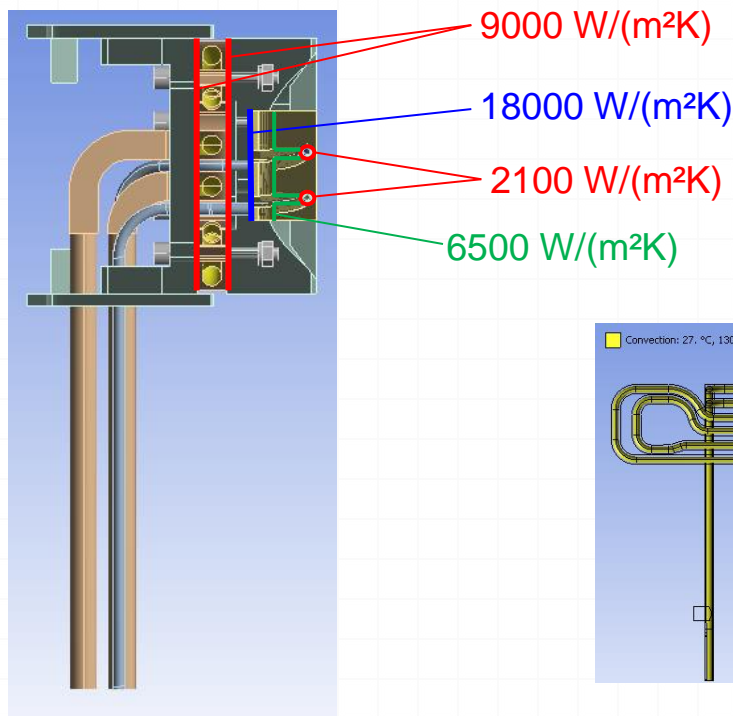
Only electric load considered: 350A DC current

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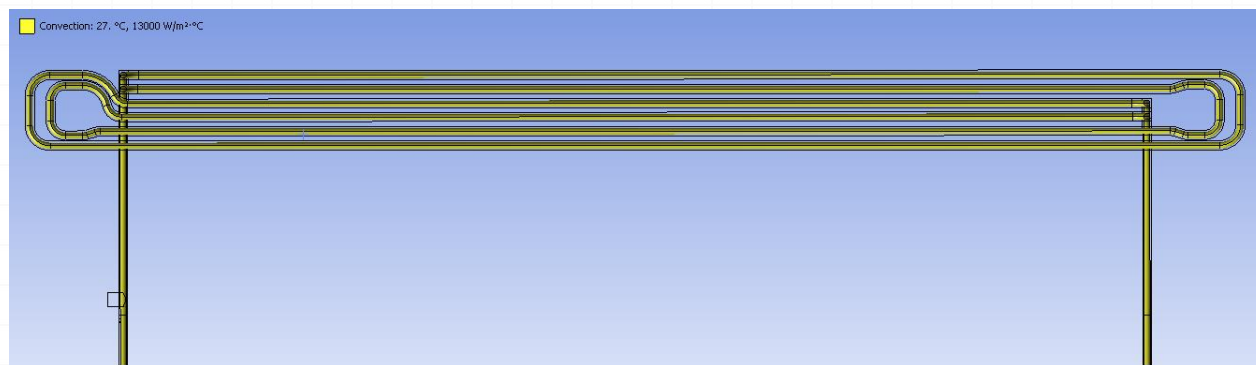
*To achieve numerical convergence, electric load applied through internal heat generation*

*Power calculated from Joule heating 350A DC at 27°C = 2.11e8 W/m<sup>3</sup>*

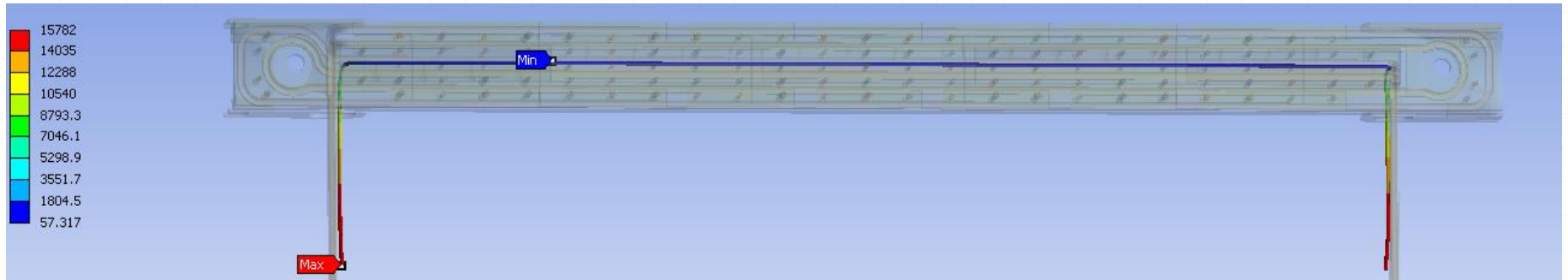
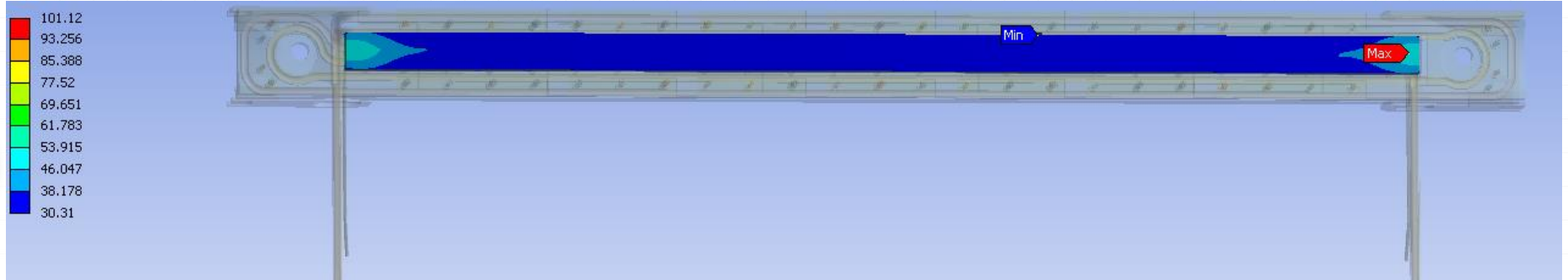
Thermal interfaces



Heat sink : convection inside cooling pipes  
13000 W/(m<sup>2</sup>K)



# 1 Wire



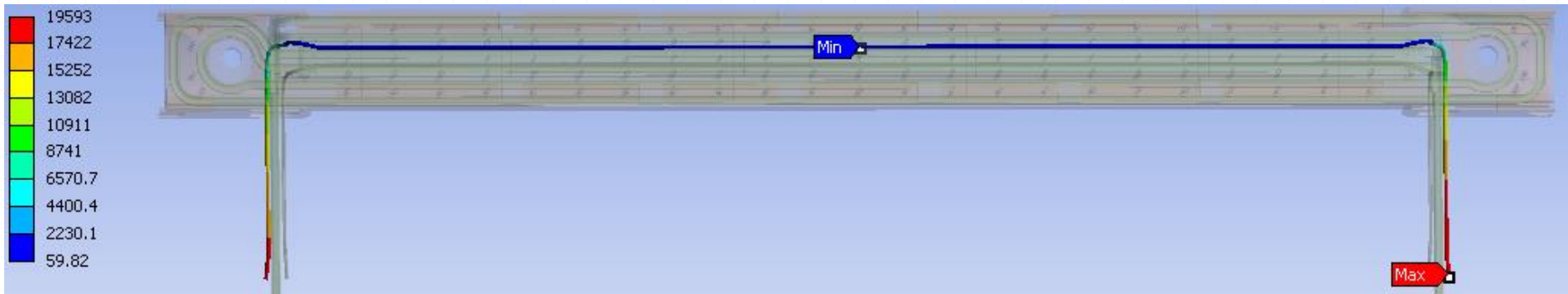
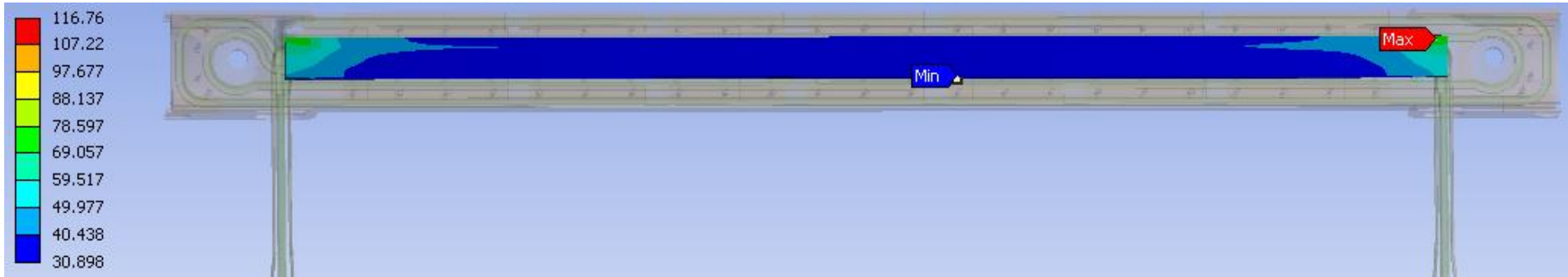
## Temperature max

- Inermet Jaw: 101.1°C
- **Wire: 15800°C**

## Average temperature

- Inermet Jaw : 34°C
- Glidcop Jaw : 31.4°C

# 2 Wires



## Temperature max

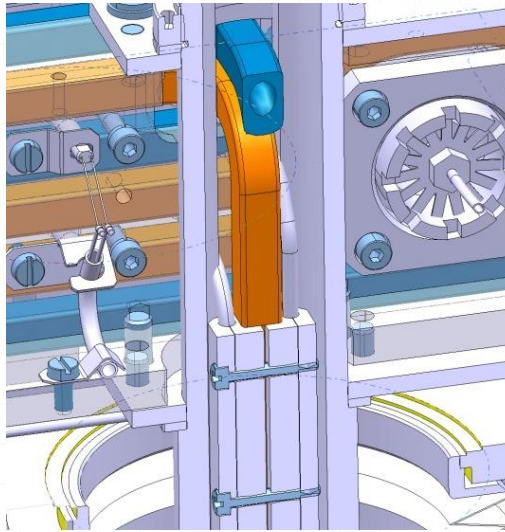
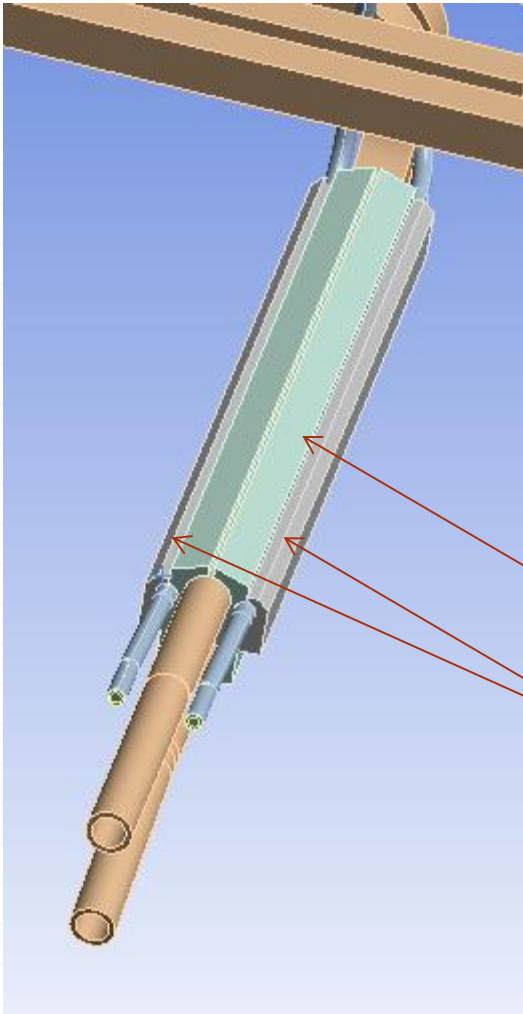
- Jaw: 116.8°C
- **Wire: 19600°C**

## Average temperature

- Inernet Jaw : 36.6°C
- Glidcop Jaw : 31°C

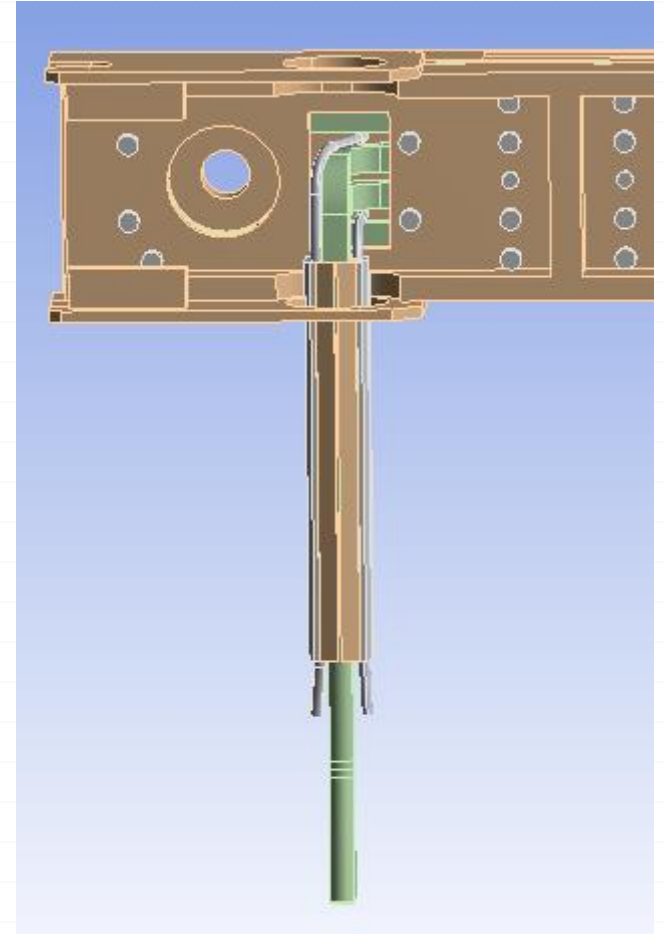


# Additional thermal bridge system



Glidcop

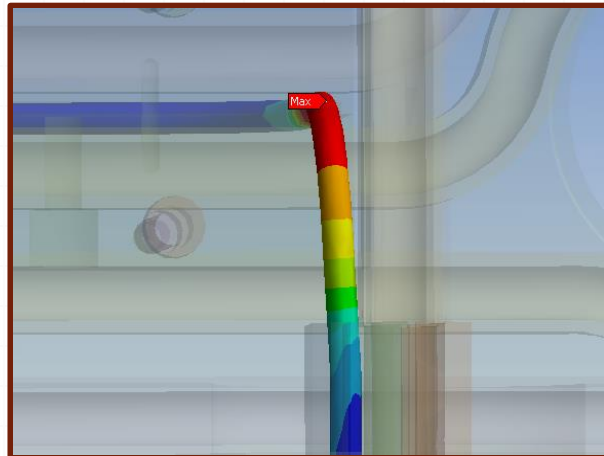
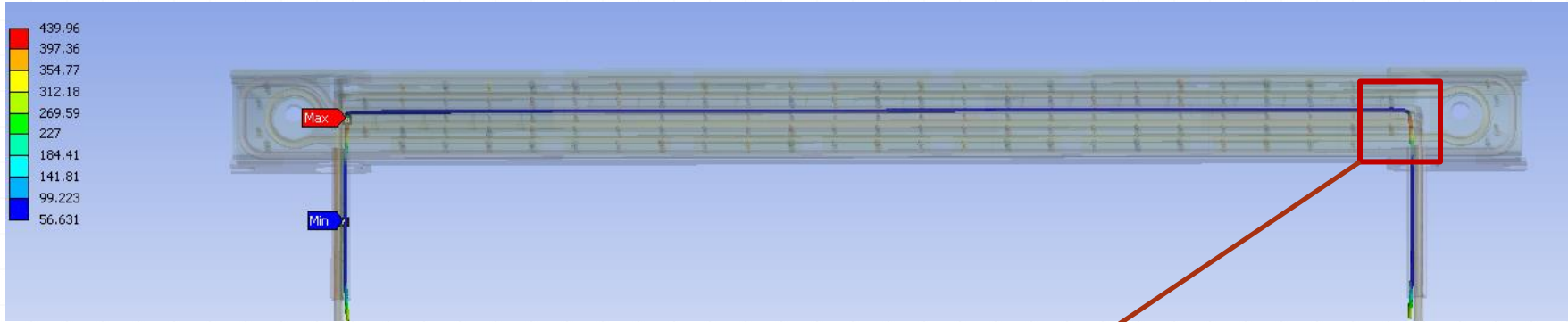
Stainless Steel



# 1 Wire – Optimized Cooling system

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## Temperature max

- Tungsten Jaw: 42.1°C
- **Wire: 440°C**

## Average temperature

- Inermet Jaw : 32.5°C
- Glidcop Jaw : 30°C

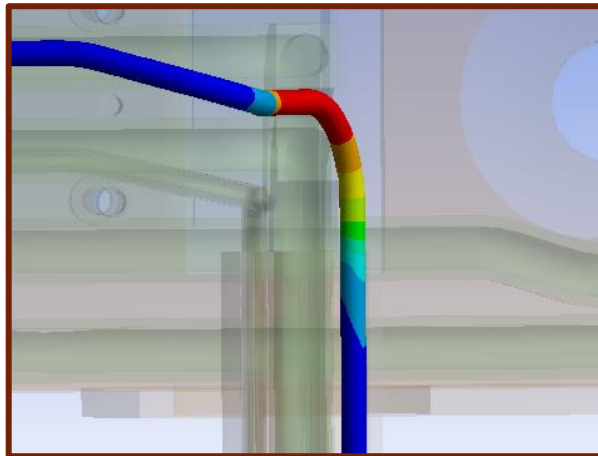
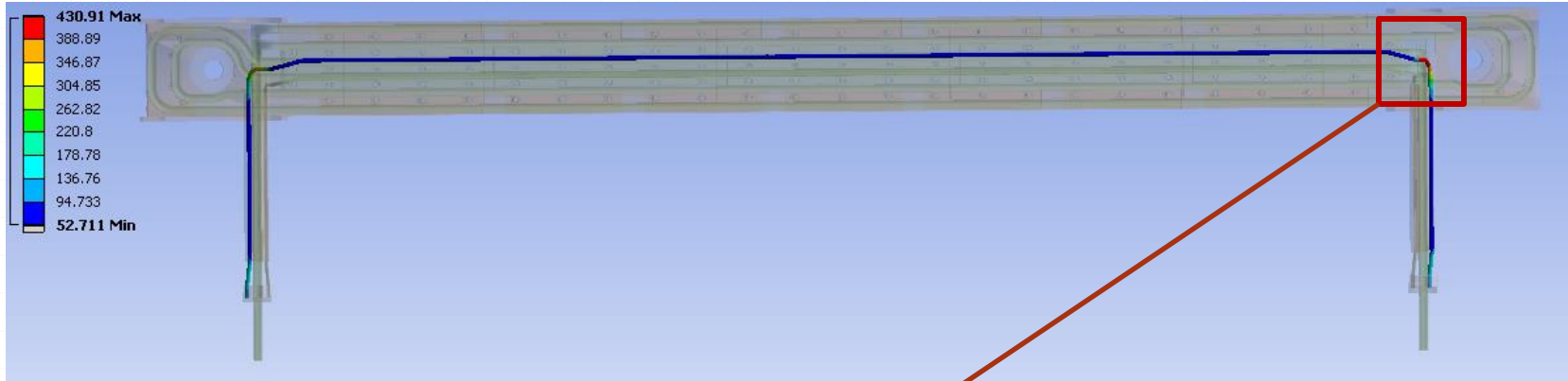




# 2 Wires - Optimized Cooling system

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## Temperature max

- Tungsten Jaw: 49.2°C
- **Wire: 431°C**

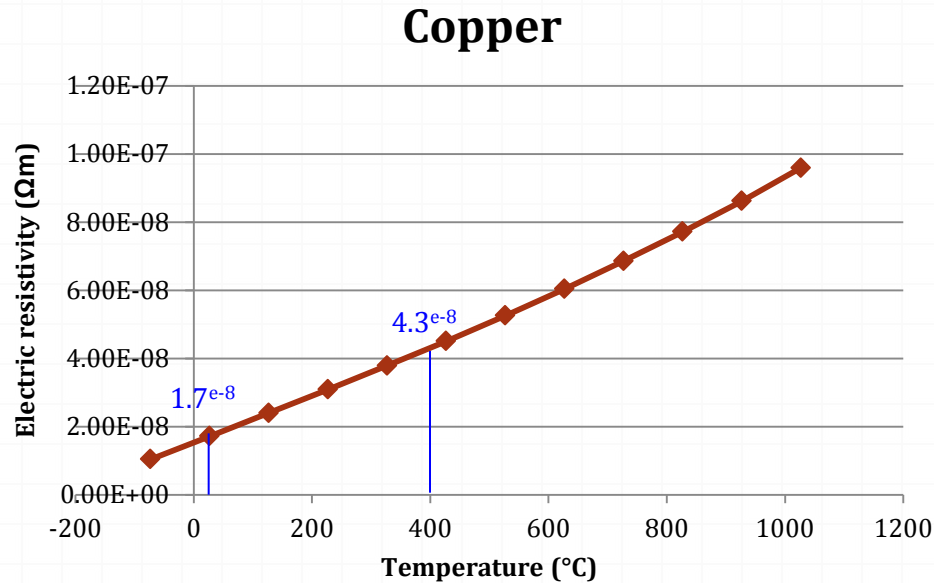
## Average temperature

- Inermet Jaw : 34.6°C
- Glidcop Jaw : 29.7°C

**350A DC not compatible with present design**

# Thermal issues

Electric resistivity not constant over temperature : **the hotter, the higher the heat generation**

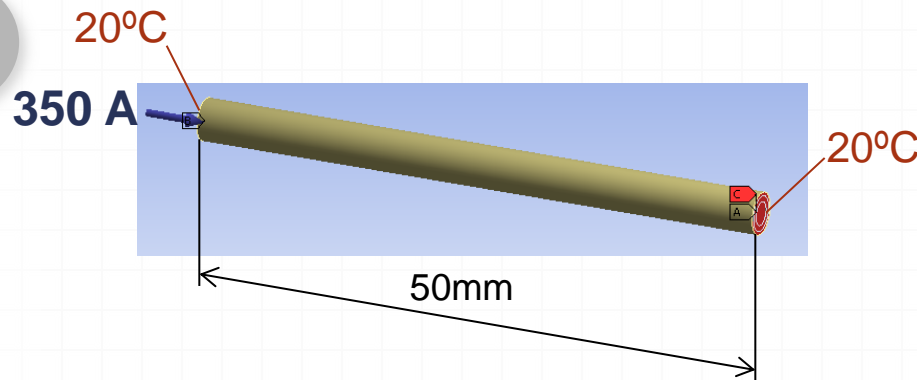
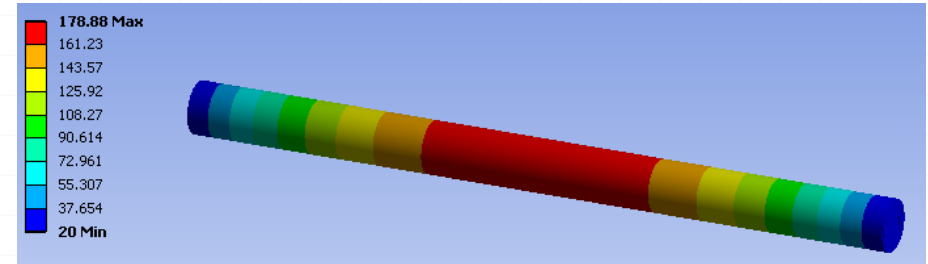


Electric resistivity at 400°C = **2.5 times the one at 27°C**

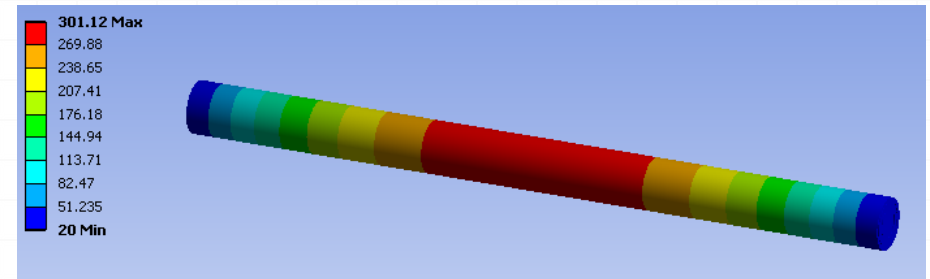
Temperatures reached are clearly underestimated

# Preliminary conclusion : Thermal issues

350 A DC with constant electric resistivity at RT



350 A DC with T-dependant electric resistivity

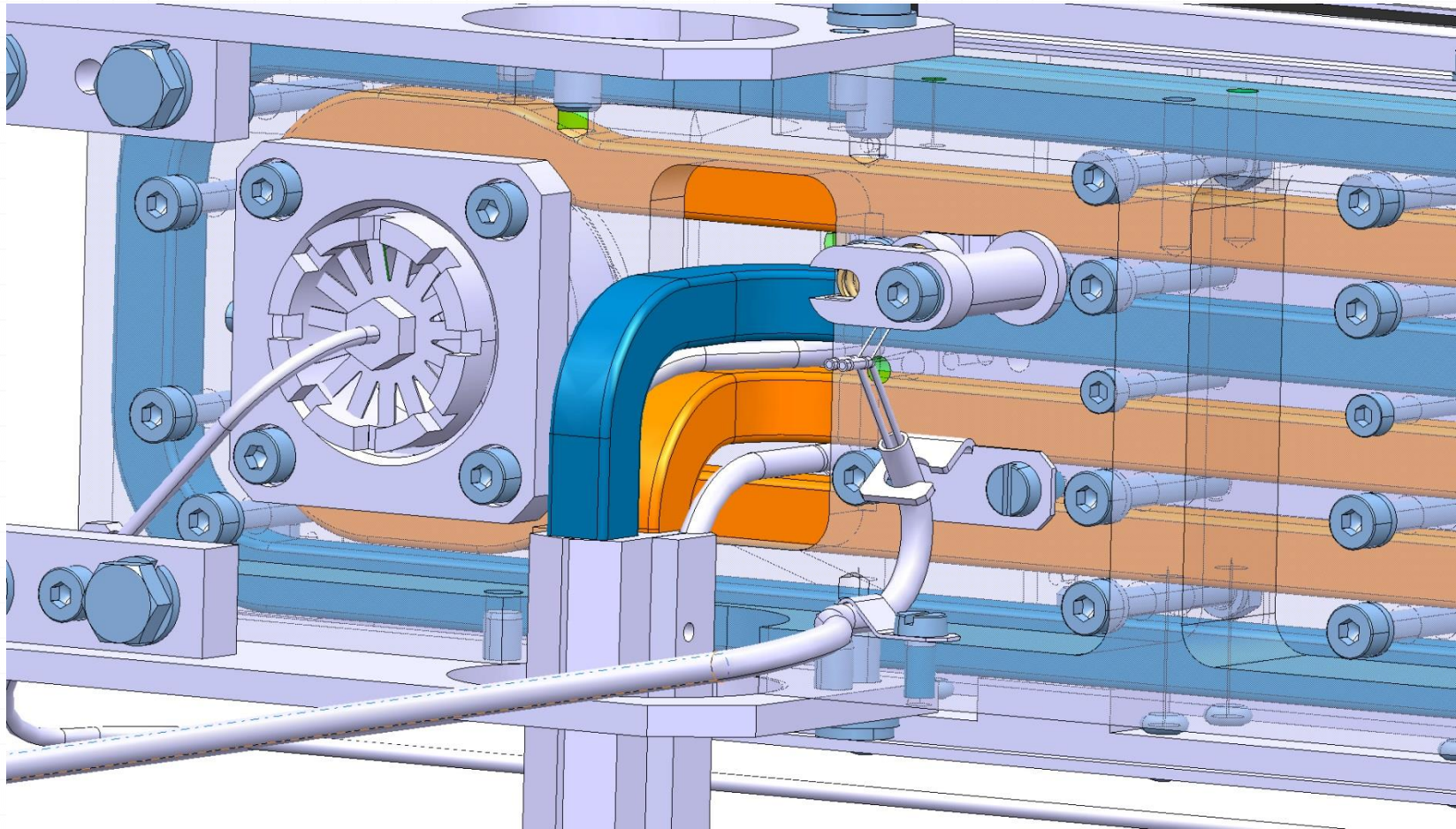


Taking into account dependancy in T :  
Strong increase of the final temperature

**Both designs not acceptable (yet !)**

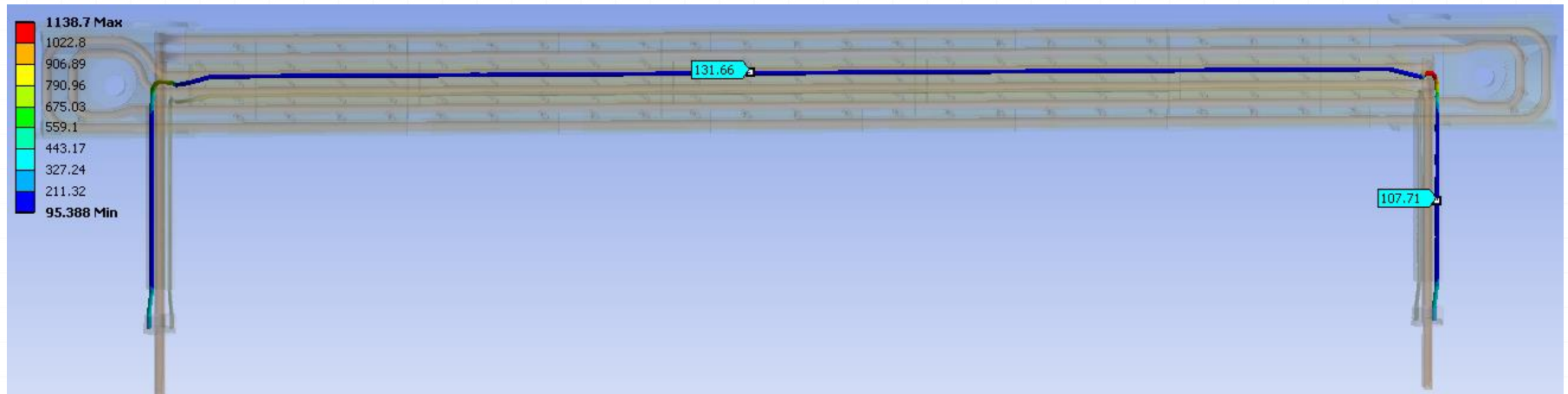
Challenge: must cool the wires in the hottest zones!

# Back-up slide



# Back-up slide

2 Wires design - Thermal load: 350 A with constant electric resistivity (at 400°C)



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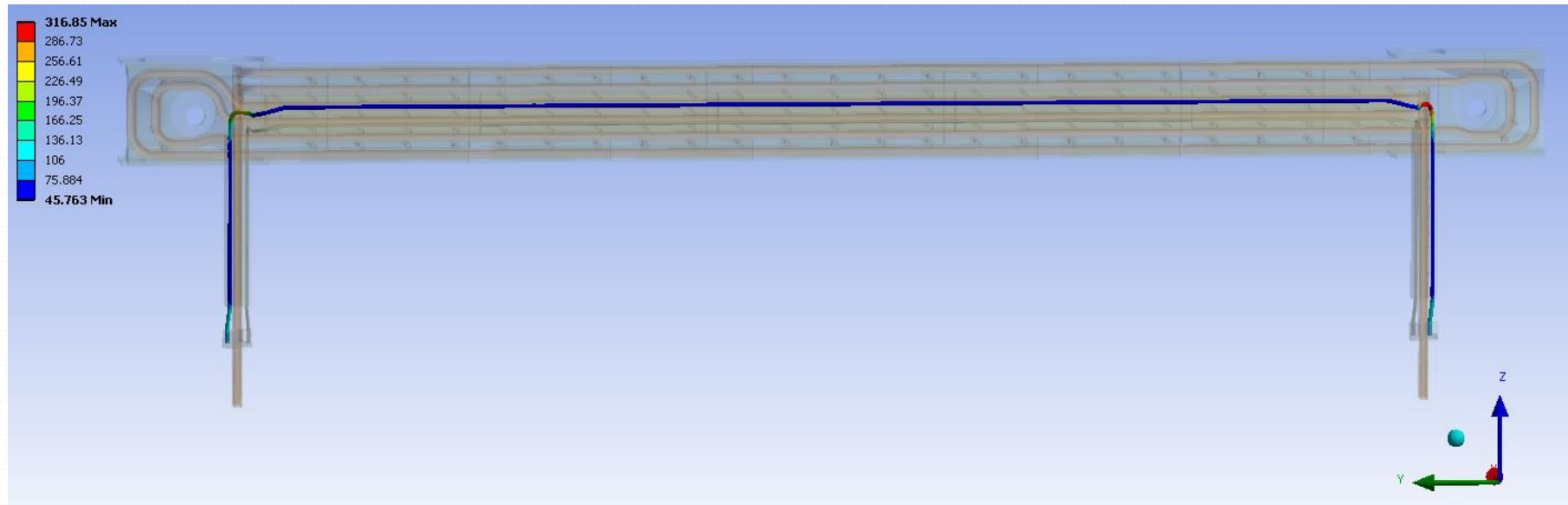
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# Back-up slide

2 Wires design - Thermal load: 300 A with constant electric resistivity (at 27°C)



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